

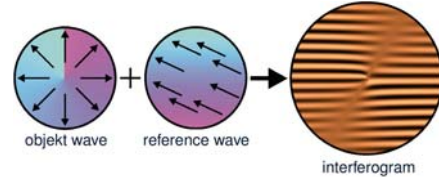
# Theoretical description of a method for simultaneous measurement of phase and arbitrary polarization

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## MOTIVATION

- New interferometric measurement for simultaneous determination of arbitrary phase and polarization distributions of an object wave
- Extension of phase shifting interferometry (PSI) to polarization and phase shifting interferometry (P&PSI) with given equidistant polarization and phase steps
- Different polarization steps allow calculation of object polarization



## THEORY

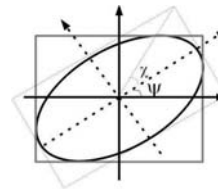
- General description of polarized light by Jones vector:

$$\vec{J} = \begin{pmatrix} E_{0x}e^{i\delta_x(x,y)} \\ E_{0y}e^{i\delta_y(x,y)} \end{pmatrix} e^{i\Phi(x,y)} \Rightarrow \vec{J} = E(x,y) \begin{pmatrix} \cos(\alpha(x,y)) \\ \sin(\alpha(x,y))e^{i\delta(x,y)} \end{pmatrix} e^{i\Phi(x,y)} \quad \text{with } \Phi' = \Phi - \delta_x, \delta = \delta_y - \delta_x \text{ and } \alpha = \arctan\left(\frac{E_{0y}}{E_{0x}}\right)$$

- Object beam: phase  $\Phi$  and polarization states described by  $\alpha$  and  $\delta$ :  $\vec{J}_O = E_O(x,y) \begin{pmatrix} \cos(\alpha(x,y)) \\ \sin(\alpha(x,y))e^{i\delta(x,y)} \end{pmatrix} e^{i\Phi(x,y)}$

- Reference beam: In the setup the different polarization states are set by a combination of a half-wave plate (HWP) and a quarter-wave plate (QWP). It's appropriate to characterize the reference Jones vector by the orientation  $\Psi$  and the ellipticity  $\chi$  of the polarization ellipse:

$$\vec{J}_R = E_R(x,y) \frac{1}{\sqrt{2}} \begin{pmatrix} \cos(\Psi + 2\chi) - i \cos(\Psi) \\ \sin(\Psi + 2\chi) - i \sin(\Psi) \end{pmatrix} e^{i\varphi(x,y)}$$



$\Psi$ : orientation,  $\chi$ : ellipticity

HWP rotated by  $\frac{\Psi}{2}$

QWP rotated by  $\Psi + \chi$

- Intensity pattern (analog to Michelson interferometric formula):

$$I = |\vec{J}_O + \vec{J}_R|^2 = I_0 \left[ 1 - \frac{V}{\sqrt{2}} (\cos(\alpha) [\cos(\Phi - \varphi) \cos(\Psi + 2\chi) - \cos(\Psi) \sin(\Phi - \varphi)] + \sin(\alpha) [\sin(\Psi + 2\chi) \cos(\Phi - \varphi + \delta) - \sin(\Psi) \sin(\Phi - \varphi + \delta)]) \right]$$

## MEASUREMENT METHOD

- The intensity  $I_j$  is measured for each polarization and phase step ( $\Psi_j, \chi_j, \varphi_j$ ). Rewrite the intensity into a vector product

$$I_j = \vec{Y}^T \vec{X}_j \quad (\text{with } a_{p/n} = \Phi \pm \alpha; \quad e_{p/n} = \Phi \pm \alpha + \delta)$$

- Thereby  $\vec{Y}$  consists of all unknown parameters ( $I_0, V, \Phi, \alpha, \delta$ ) whereas  $\vec{X}$  includes the adjustable reference values ( $\Psi_j, \chi_j, \varphi_j$ )

- With the matrix  $\hat{A}$  the equation can be solved for  $\vec{Y}$ :

$$\vec{Y} = \hat{A}^{-1} \sum_{j=1}^N \vec{X}_j I_j; \quad (\text{with } \hat{A} = \sum_{j=1}^N \hat{A}_j = \sum_{j=1}^N \vec{X}_j \vec{X}_j^T)$$

Only for specified values of  $\Psi_j \in [0; \pi]$ ;  $\chi_j \in [-\pi/4; \pi/4]$ ;  $\varphi_j \in [0; 2\pi]$   $\hat{A}$  is invertible.

- Different evaluation algorithms are possible. For each the polarization and phase steps are equidistant and there must be at least  $N \geq 9$  images.

–“Non averaging” algorithm: phase steps:  $\delta_\varphi = \frac{2\pi}{N_\varphi}$ , possible for  $N_{\Psi,\chi} \geq 2$  and  $N_\varphi \geq 3$

–“Averaging” algorithm: phase steps:  $\delta_\varphi^* = \frac{2\pi}{N_\varphi - 1}$ , possible for  $N_\chi \geq 2, N_\Psi \geq 3$  and  $N_\varphi \geq 4$

→ results in Poster Nr.2

$$\vec{Y} = \frac{-I_0 V}{4\sqrt{2}} \begin{pmatrix} -\frac{4\sqrt{2}}{V} \\ -\sin(a_n) - \sin(a_p) + \sin(e_p) - \sin(e_n) \\ -\sin(a_n) - \sin(a_p) - \sin(e_p) + \sin(e_n) \\ \cos(a_n) + \cos(a_p) + \cos(e_p) - \cos(e_n) \\ \cos(a_n) + \cos(a_p) - \cos(e_n) + \cos(e_p) \\ \cos(a_n) + \cos(a_p) + \cos(e_n) - \cos(e_p) \\ \cos(a_n) + \cos(a_p) - \cos(e_n) + \cos(e_p) \\ \sin(a_n) + \sin(a_p) - \sin(e_p) + \sin(e_n) \\ \sin(a_n) + \sin(a_p) + \sin(e_p) - \sin(e_n) \end{pmatrix} \vec{X}_j = \begin{pmatrix} 1 \\ \cos(\varphi_j - \Psi_j) \\ \cos(\varphi_j + \Psi_j) \\ \sin(\varphi_j - \Psi_j) \\ \sin(\varphi_j + \Psi_j) \\ \cos(\varphi_j - (\Psi_j + 2\chi_j)) \\ \cos(\varphi_j + (\Psi_j + 2\chi_j)) \\ \sin(\varphi_j - (\Psi_j + 2\chi_j)) \\ \sin(\varphi_j + (\Psi_j + 2\chi_j)) \end{pmatrix}$$

$$I_0 = Y_1; \quad \Phi + \delta = \arctan\left(\frac{Y_3 - Y_2}{Y_4 - Y_5}\right); \quad \Phi = \arctan\left(\frac{Y_8 + Y_9}{Y_6 + Y_7}\right);$$

$$\alpha = \arctan\left(\sqrt{\frac{(Y_3 - Y_2)^2 + (Y_4 - Y_5)^2}{(Y_6 + Y_7)^2 + (Y_8 + Y_9)^2}}\right); \quad V = \frac{\sqrt{(Y_3 - Y_2)^2 + \dots + (Y_6 + Y_7)^2}}{Y_1}$$

$$\alpha \in [0; \frac{\pi}{2}], \delta \in [0; \pi] \text{ and } \Phi \in [0; 2\pi]$$

## MEASUREMENT SETUP

- Folded Mach-Zehnder interferometer allows almost normal ( $5^\circ$ ) incidence on the mirrors, so influences on the polarization are suppressed.
- With a Wollaston prism as beamsplitter (BS) the intensity ratio between object and reference arm is adjustable and therefore the visibility of the interferogram can be improved.
- Polarization shifting is enabled by rotating the HWP and QWP in the reference arm. For phase shifting mirror M1 in the object arm is moveable.
- To conserve the incident polarization distributions a special phase grating is used as beam combiner (BC).

